

Acoustic Consultancy Report

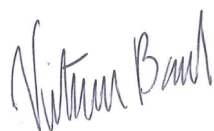
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Mechanical Plant Assessment

Report Prepared For

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Bath Asu
23 April 2026

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i) Executive Summary

LCP has been commissioned to conduct an appraisal of the acoustic performances of the proposed office development located at Bath ASU, in Corsham Science Park.

This acoustic design report sets out criteria recommended by LCP for a comfortable and effective working environment, and then assesses the current proposals to those criteria. It is principally concerned with the following aspect of the design:

Design Aspect(s) Assessed in This Report

Internal ambient noise levels;

External ambient noise levels.

The design as proposed and assessed will achieve the required criteria provided the details in Section 5 and 6 of this report is implemented.

ii) Document History

Issue	Date	Issue Details	Issued By	Checked By
1	10 th February 2026	Initial Issue	VB	MB
2	23 rd April 2026	Internal Plant Assessment	VB	RM

1. Introduction

LCP has been commissioned to conduct an appraisal of the acoustic performances of the proposed office development located at Bath ASU, in Corsham Science Park.

This acoustic design report sets out criteria recommended by LCP for a comfortable and effective working environment, and then assesses the current proposals to those criteria. It is principally concerned with the following aspect of the design:

Design Aspect(s) Assessed in This Report

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2. Survey

2.1. Site Description

The site layout together with the measurement position is shown in the drawing contained within Appendix A.

2.2. Receiver Location

The site was surveyed to determine the location of the most affected receiver.

The nearest residential receiver to the plant area are the double storey dwellings along Westwells Road, approximately 160m to the south of the site. This noise impact assessment also considers the double storey dwellings along The Links, approximately 168m to the west however these properties are screen by existing neighbouring commercial buildings. The commercial warehouse building of Corsham Building Plastics is in close proximity to the proposed plant. This is shown in the site plan in Appendix A.

2.3. Local Noise Climate

The predominant local noise sources were road traffic, including HGV's, along Westwells Road and Park Lane, and to a lesser extent, distant road traffic noise from local road networks.

2.4. Measurements

The noise monitoring took place from 06:00hrs to 09:00hrs on the 28th of January 2026. The measurement period was considered sufficient to establish the representative background sound levels corresponding to the operational period of the plant. The weather conditions monitored during the survey are shown in the following table.

Table 1: Weather Conditions at Measurement Location

Weather	Value
Average Wind Speed	1m/s
Wind Direction	North-west
Cloud Cover	10%

Weather	Value
Temperature	3°C
Precipitation	None

2.5. Measurement Results

The measured statistical broad-band sound pressure levels are shown within Appendix C. The representative background sound level(s) obtained, between 06:00hrs to 09:00hrs considered to be the most noise sensitive, being as follows:

Table 2: Representative background sound levels, dB re 2×10^{-5} Pa

Measurement Position	$L_{A90, 15 \text{ mins}}$ Day*	$L_{A90, 15 \text{ mins}}$ Night*
MP1	54	41

* Day and Night periods are defined as between 07:00 - 23:00 and 23:00 - 07:00 respectively.

3. Evaluation of External Design Criteria

3.1. Residential Design Criterion

3.1.1. BS4142:2014

BS4142:2014 states that the significance of sound of an industrial and/or commercial nature depends upon both the margin by which the rating level of the specific sound source exceeds the background sound level and the context in which the sound occurs.

Table 3: BS4142 assessment based upon rating level

Difference between background noise and rating levels	Assessment
+ 10 dB	Indication of a significant adverse impact
+ 5 dB	Indication of an adverse impact
0 dB	Indication of low impact

Certain acoustic features can increase the significance of impact. The specific sound level should be corrected if a tone, impulse or other acoustic feature is expected to be present.

Table 4: Corrections for acoustic features, subjective method

Acoustic Feature	Correction, dB		
	Just Perceptible	Clearly Perceptible	Highly Perceptible
Tonality	2	4	6

Acoustic Feature	Correction, dB		
	Just Perceptible	Clearly Perceptible	Highly Perceptible
Impulsivity	3	6	9
Other Characteristics	3		
Intermittency	3		

Typically the acoustic feature correction would not be expected to exceed 10dB.

Where the level of uncertainty could affect the conclusion, take reasonably practicable steps to reduce the level of uncertainty.

3.1.2. World Health Organisation (WHO) Guidelines for Community Noise (1999)

The WHO's 'Guidelines for Community Noise' gives the following relevant noise criteria:

Table 5: Guideline values for community noise, from Guidelines for Community Noise (WHO, 1999)

Specific Environment	$L_{Aeq, T}$ dB	Time Base (hours)	$L_{Amax, fast}$ dB
Outdoor living area (serious annoyance, daytime and evening)	55	16	-
Outdoor living area (moderate annoyance, daytime and evening)	50	16	-
Dwelling, indoors	35	16	-
Inside bedrooms	30	8	45
Outside bedrooms	45	8	60
Outdoors in parkland and conservation areas*	-	-	-

* Existing quiet outdoor areas should be preserved and the ratio of intruding noise to natural background sound should be kept low

The WHO's 'Guidelines for Community Noise' also gives the following general guidance on the expected sound insulation performance of a façade with a partly open window, it states that:

"At night, sound pressure levels at the outside facades of the living spaces should not exceed 45 dB L_{Aeq} and 60 dB L_{Amax} , so that people may sleep with bedroom windows open. These values have been obtained by assuming that the noise reduction from outside to inside with the window partly open is 15 dB."

3.1.3. BS8233:2014

The criteria offered in BS8233 for residential buildings are largely based on the recommendations made in the Guidelines for Community Noise.

Using the general guidance from above, on the expected sound insulation performance of a façade with a partly open window, the criteria shown in the table below have been adapted from the criteria offered in table 4 of BS8233 in order to obtain acceptable external noise levels.

The noise levels shown should be treated as overall noise levels, i.e., the combination of all existing noise levels at the site, and noise levels from any proposed plant or activity.

Table 6: External ambient noise levels for dwellings, based on BS8233, dB re 2×10^{-5} Pa

Activity	Location	Time period	
		07:00 to 23:00	23:00 to 07:00
Resting	Living Room	50 $L_{Aeq, 16 \text{ hour}}$	-
Dining	Dining Room/area	55 $L_{Aeq, 16 \text{ hour}}$	-
Sleeping (daytime resting)	Bedroom	50 $L_{Aeq, 16 \text{ hour}}$	45 $L_{Aeq, 8 \text{ hour}}$

In addition to the above criteria, BS8233 goes on to say *"For traditional external areas that are used for amenity space, such as gardens and patios, it is desirable that the external noise level does not exceed 50 $L_{Aeq, T}$, with an upper guideline value of 55 dB $L_{Aeq, T}$ which would be acceptable in noisier environments."*

The above criteria are in line with the recommendations made in WHO's 'Guidelines for Community Noise'.

3.1.4. Recommended Residential Design Rating Level

On the basis of the above the recommended residential design rating level should therefore be:

Residential Design Rating Level

Representative $L_{A90, 15 \text{ mins}}$ dB

3.2. Commercial Design Criterion (BS8233:2014)

External design criteria for non-residential buildings have been derived from BS8233:2014. Using the general guidance from WHO, on the expected sound insulation performance of a façade with a partly open window, the criteria shown in the table below have been adapted from the criteria offered in tables 2 and 6 of BS8233 in order to obtain acceptable external noise levels.

The noise levels shown should be treated as overall noise levels, i.e., the combination of all existing noise levels at the site, and noise levels from any proposed plant or activity.

Table 7: External ambient noise levels for non-domestic buildings, based on BS8233, dB re 2×10^{-5} Pa

Activity	Location	Design Level $L_{Aeq, 16 \text{ hr}}$
Speech or telephone communications	Department store, cafeteria, canteen, kitchen	70
	Concourse, corridor, circulation space	70

Activity	Location	Design Level $L_{Aeq, 16 \text{ hr}}$
Study and work requiring concentration	Library, gallery, museum	65
	Staff/meeting room, training room	60
	Executive office	55
	Open plan office	65
Listening	Place of worship, counselling, meditation, relaxation	50

3.2.1. Recommended Commercial Design Rating Level

On the basis of the above the recommended commercial design rating level should therefore be:

Commercial Design Rating level
$L_{Aeq, T}$ 70 dB

3.3. Design Rating Levels

The design levels to be adopted for this project are set out in the table below.

Table 8: Design rating levels, dB re 2×10^{-5} Pa

Receiver Premises	Approximate Distance (m)	Design Level (Day), $L_{Aeq, 16 \text{ hr}}$	Design Level (Night), $L_{Aeq, 8 \text{ hr}}$
Nearest residential window of dwellings along Westwells Road	160	54	41
Nearest residential window of dwellings along The Links	168	54	41
Nearest commercial window	19	70	-

4. Evaluation of Internal Design Criteria

4.1. Client Specifications

The client has specified the below design criteria for internal spaces.

Table 9: Internal Design Criteria

Space	NR
Offices/Meeting Rooms	35
WC/Breakrooms	45
GMP Areas	50
Technical Area	80

Space	NR
UNC GF corridor	60
UNC Mezz corridors/lobbies	40
UNC Mezz WCs and breakroom	45

4.2. Reverberation Time

BS8233: 2014 states that the optimum reverberation time for a space depends on the purpose and volume of the space and guide values for reverberation times for rooms of different volumes can be found in standard texts.

The following table is taken from the Association of Interior Specialist (AIS) 'A guide to office acoustics'.

Table 10: Reverberation time criteria at 500Hz in unoccupied rooms for speech, seconds

Room Volume m ³	Reverberation Time
50	0.4
100	0.5
200	0.6
500	0.7
1000	0.9
2000	1.0

5. External Plant Assessment

5.1. Current Design

The proposed plant shall comprise of two air handling units (AHU's), same make and model numbers, and one MVHR unit, all three with associated fresh air in and discharge terminals.

Nine VRF units, six ODU units and two extract fans systems (four fans in total however two fans will run in parallel at a reduced load, should one fan fail the remaining fan will ramp up to maintain total airflow) , together with the AHU's and MVHR units shall be located externally at ground level of the façade of the site. The proposed plant location is provided in Appendix B. Attenuators are proposed and their location and insertion losses used in this assessment is provided in Appendix D.

The guidance contained in this report is given on the basis that the operational period of the plant may potentially be continuous between 06:00hrs and 22:00hrs.

5.2. Calculated Results

Calculations of the predicted noise levels have been carried out with the appropriate corrections for geometric attenuation, barrier effect, reflective surfaces and multiple source addition.

A 3dB(A) acoustic feature correction has been applied to the results in the following table to account for any intermittency.

The design rating levels to be adopted for this project, together with the predicted noise levels, are set out in the following table.

Table 11: Design and predicted rating levels, dB re 2×10^{-5} Pa

Receiver Premises	Approximate Distance, (m)	Design Level (Day), $L_{Aeq, 16 \text{ hr}}$	Design Level (Night), $L_{Aeq, 8 \text{ hr}}$	Predicted Level, dB $L_{Aeq,T}$
Nearest residential window of dwellings along Westwells Road	160	54	41	41
Nearest residential window of dwellings along The Links	168	54	41	39
Nearest commercial window	19	70	-	59

Plant noise level data used in this assessment are contained within Appendix D.

Calculations are shown within Appendix E.

6. Internal Plant Assessment

The calculated internal ambient noise level contribution from the proposed AHU's and CAV units are shown in the following table. When the MVHR schematic with air flows has been confirmed these may be reviewed.

The calculations assume a grille area of 400mm².

The reverberation time of the spaces should achieve the criteria provided in table 10.

The building services layout drawing is shown in Appendix B.

Attenuators are essential in the design and the location and insertion losses are provided in table 15. Following this acoustic review further attenuators are advised in addition to the proposed attenuators.

It is critical that all ductwork is externally lagged and that the 0.5m flexible connection is acoustically lined. The flexible duct and grille should be connected by a 90° lined shallow plenum.

Table 12: Internal ambient noise levels contribution from internal building services noise, NR

Space	Criteria, NR	Predicted, NR
SP2-015 Manufacture 1	50	48
SP2-013 Manufacture 2	50	48
SP2-014 Assembly Check and Prep	50	48
SP2-004 Labelling/Bagging	50	50
SP2-003 Grade D Pal	50	42

Space	Criteria, NR	Predicted, NR
SP2-021 Grade C Pal	50	48
SP2-020 Grade D Pal	50	50
SP2-019 Grade D/C Cleaning Store	50	39
SP2-005 Grade D Cleaning Store	50	45
SP2-018 Debox	50	48

7. Conclusion

LCP has been commissioned to conduct an appraisal of the acoustic performances of the proposed office development located at Bath ASU, in Corsham Science Park.

This acoustic design report sets out criteria recommended by LCP for a comfortable and effective working environment, and then assesses the current proposals to those criteria. It is principally concerned with the following aspect of the design:

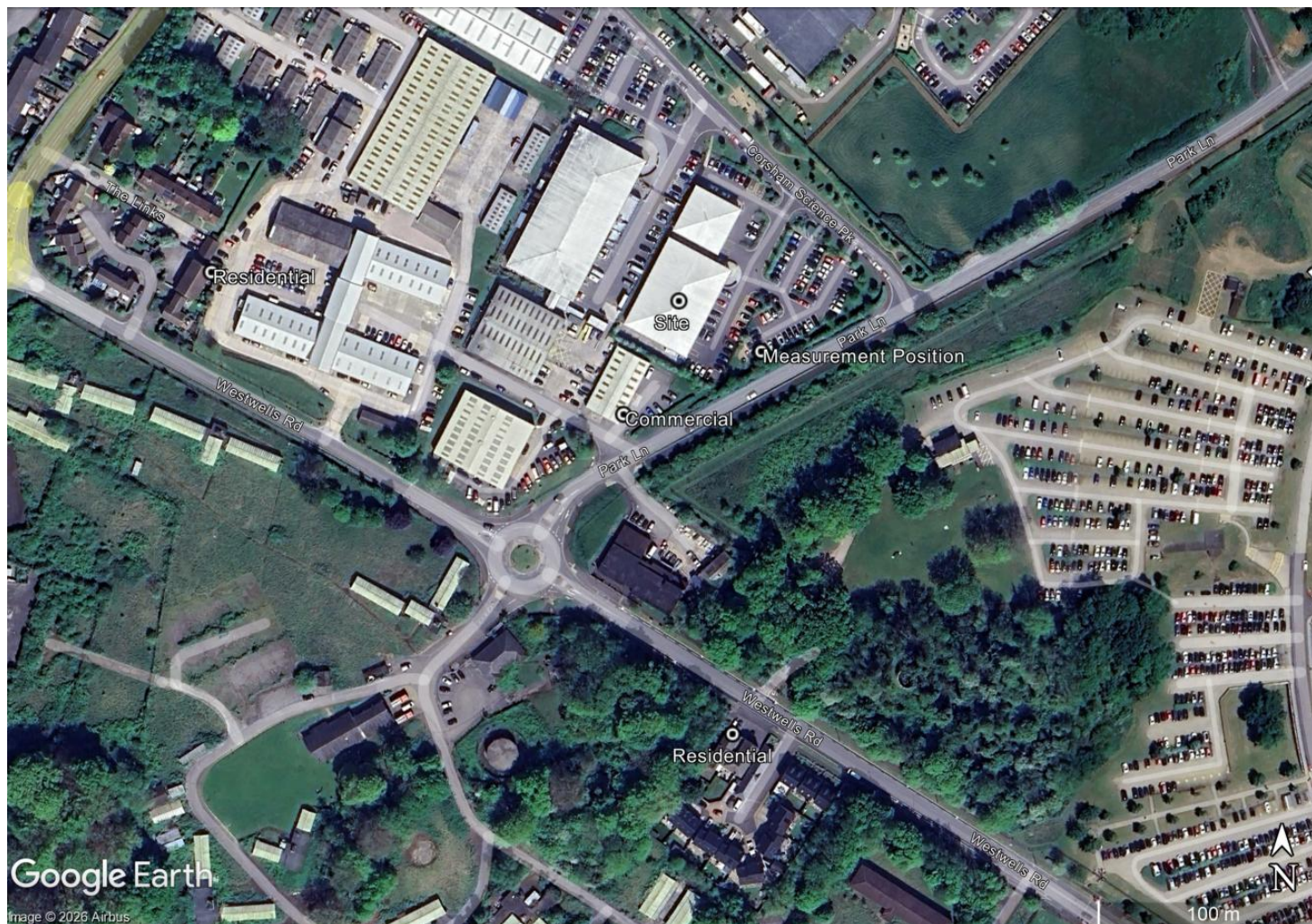
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Internal ambient noise levels;

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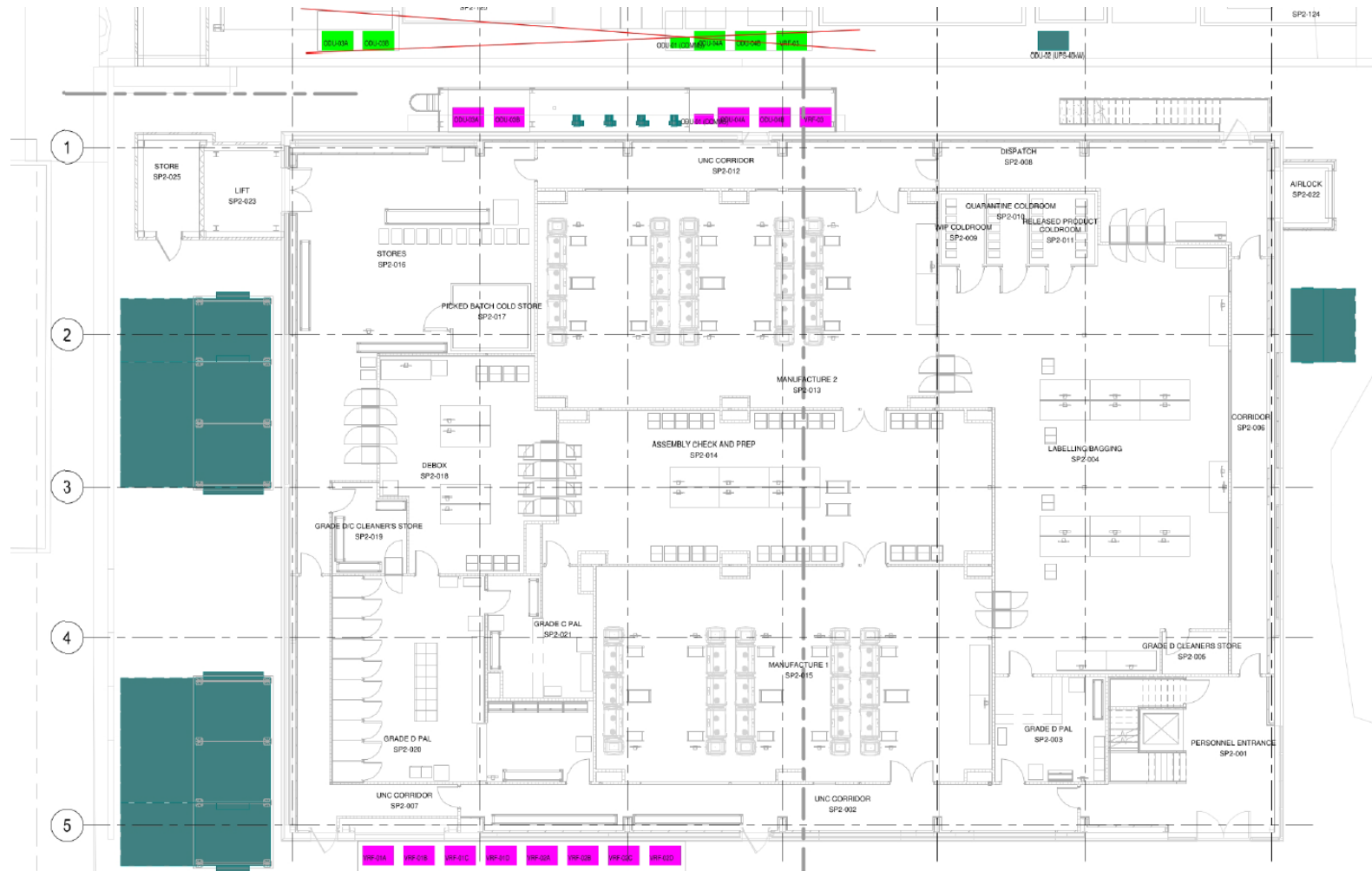
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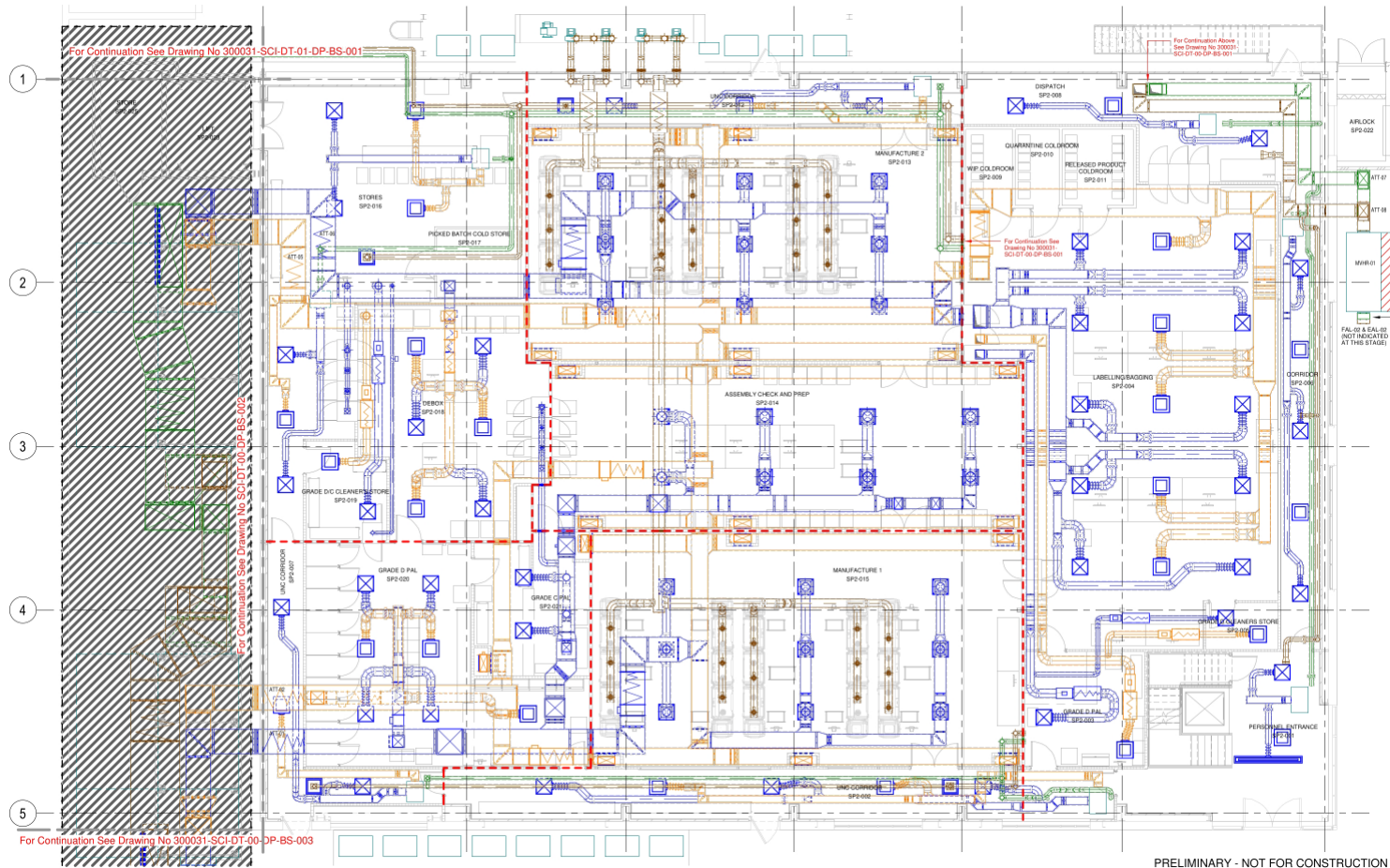
Appendix A: Site Plan



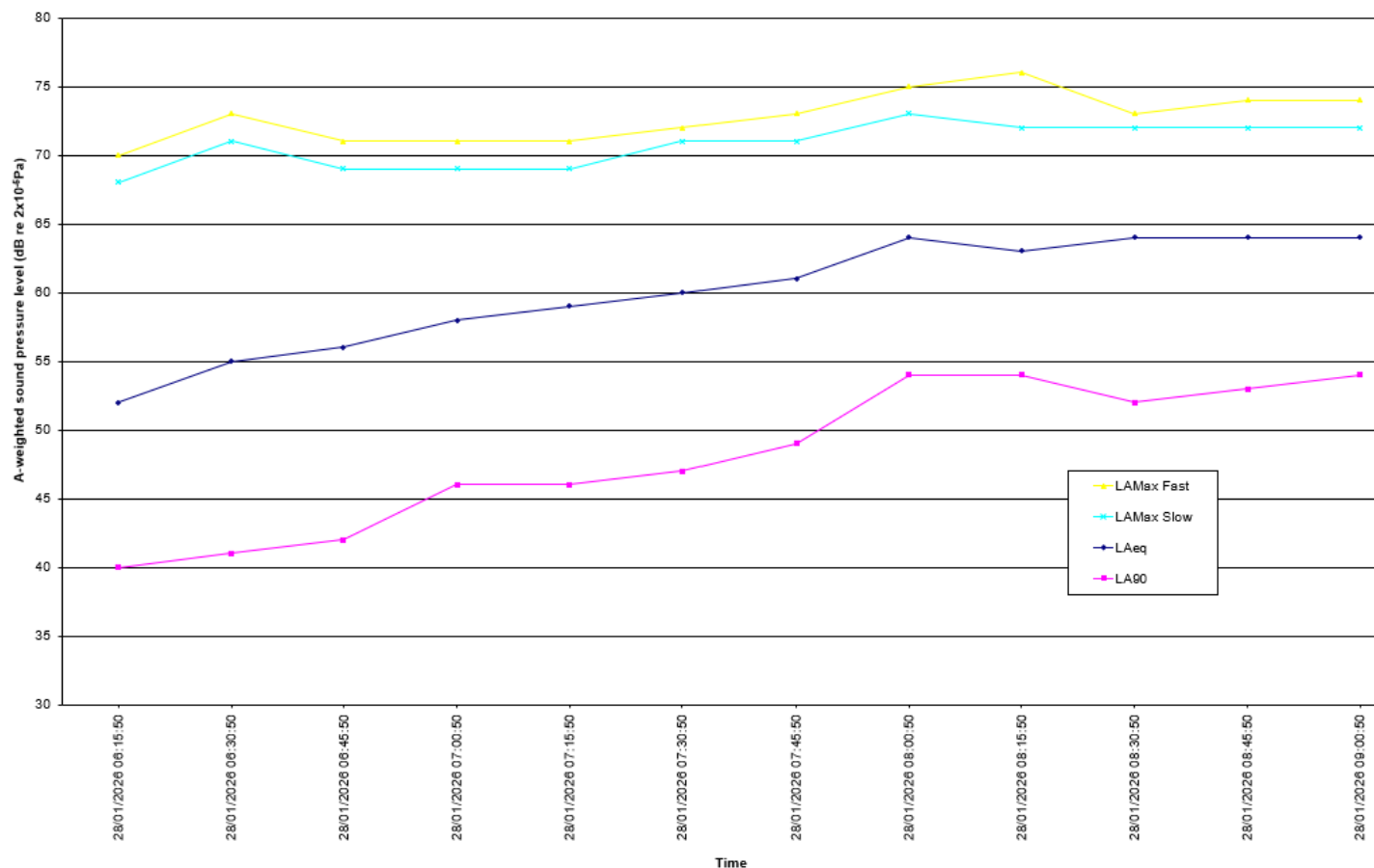
Approximate measurement position (Latitude & Longitude) 51°25'23.92"N, 2°13'12.63"W.

Appendix B: Plant Location





Appendix C: Measurement Data



Sound pressure level measurements were obtained using the following instrumentation complying with the Class 1 specification of BS EN 61672:2003

- Svantek 959 Sound Level Meter S/N: 11207 (next cal due 28/07/2027) Start gain +1.73 End gain +1.69
- Svantek pre-amplifier SV12L S/N: 49860 with GRAS microphone capsule 40AE S/N: 215511

Calibration checks were made prior to and after completion of measurements using a Svantek SV30A calibrator, S/N: 10890 (next cal due 04/02/2026) complying with Class 1 specification of BS EN 60942:2003, calibration level 114.0 dB @ 1.0 kHz. All acoustic instrumentation carried current manufacturer's certificates of conformance.

Appendix D: Plant Data

Plant noise data used in the preceding assessment follow.

Table 13: Manufacturer's plant sound power data, dB re 10^{-12} W

Plant	Octave Band Centre Frequency (Hz)								L _{WA}
	63	125	250	500	1k	2k	4k	8k	
AHU – Fresh air in	100	83	89	80	73	65	54	48	84
AHU – Discharge	92	81	91	88	89	89	85	82	95
AHU – Supply	102	84	93	82	74	63	43	32	86
AHU – Extract	86	76	83	77	70	59	52	47	78
AHU – Case radiated	92	78	75	61	61	60	53	39	71
MVHR – Fresh air in	70	70	72	65	55	47	37	36	66
MVHR – Discharge	71	73	77	74	75	73	69	69	80
MVHR – Extract	70	69	70	65	56	48	43	45	66
MVHR – Supply	72	73	78	75	75	74	70	70	80
MVHR – Case radiated	65	59	60	51	49	51	38	27	57
Extract fan - Inlet	85	90	94	101	93	83	77	74	99
CAV-S08	48	52	54	53	50	46	40	31	59
CAV-R08	48	53	54	54	51	46	40	31	59
CAV-S06	70	66	64	63	62	61	59	55	68
CAV-R06	71	67	64	63	62	61	59	55	68
CAV-TH-S02	42	46	48	47	44	40	34	25	49
CAV-TH-S03	41	46	47	47	44	39	33	24	48
CAV-S10	45	50	51	51	48	43	37	28	52
CAV-R10	45	49	51	50	47	43	37	28	52
CAV-S09	44	48	49	49	46	42	36	27	51
CAV-R09	46	50	52	52	49	44	38	29	53

Plant	Octave Band Centre Frequency (Hz)								L _{WA}
	63	125	250	500	1k	2k	4k	8k	
CAV-S07	72	66	62	60	59	58	57	54	65
CAV-R07	72	66	62	60	59	58	57	55	65
CAV-S05	73	69	67	65	64	63	61	57	70
CAV-R05	69	66	64	63	62	60	58	54	67
CAV-S04	73	67	64	62	61	60	58	56	67
CAV-R04	72	66	63	62	61	60	58	55	67
CAV-S02	71	67	65	64	63	62	59	56	69
CAV-R02	71	67	65	64	63	62	60	56	69
CAV-TH-S01	41	46	47	47	44	39	33	24	48
CAV-S03	67	62	58	57	56	55	53	51	62
CAV-R03	68	62	59	57	56	55	54	51	62
CAV-S01	73	69	67	65	64	63	61	57	70
CAV-R01	69	66	64	63	62	60	58	54	67
CAV-TH-S04	34	38	39	39	36	32	26	17	41
CAV-E01 to CAV-E15	42	46	48	47	44	40	34	25	49
CAV-E16 to CAV-E30	42	46	48	47	44	40	34	25	49

Table 14: Manufacturer's plant sound pressure data, dB re 2x10⁻⁵ Pa

Plant	Distance (m)	Octave Band Centre Frequency (Hz)								L _{PA}
		63	125	250	500	1k	2k	4k	8k	
ODU (Daikin RZAG35B)	1	52	52	51	48	41	37	29	25	48
VRF (Daikin RXYA16A)	1	69	65	62	63	58	55	55	46	65
Extract fan - Discharge	1	33	54	69	85	82	73	67	62	87
Extract fan - Case radiated	1	35	49	57	70	65	56	50	43	72

Table 15: Proposed attenuators insertion losses

Plant	Location	Octave Band Centre Frequency (Hz)							
		63	125	250	500	1k	2k	4k	8k
AHU	Fresh air in	2	5	10	17	20	15	11	7
AHU	Discharge	2	5	10	17	20	15	11	7
AHU	Supply Primary	3	7	13	23	27	20	14	9
AHU	Supply Secondary	3	5	11	21	17	11	8	5
AHU	Extract	1	4	7	12	14	11	7	5
MVHR	Fresh air in	2	6	10	17	22	17	13	8
MVHR	Discharge	2	6	10	17	22	17	13	8
MVHR	Supply	5	10	15	20	24	17	13	9
MVHR	Extract	5	10	15	20	24	17	13	9
CAV- S04	Supply	2	3	8	22	38	16	14	13
CAV-R04	Extract	2	3	8	22	38	16	14	13
CAV- S02	Supply	2	3	8	22	38	16	14	13
CAV-R02	Extract	2	3	8	22	38	16	14	13
CAV- S07	Supply	2	3	8	22	38	16	14	13
CAV-R07	Extract	2	3	8	22	38	16	14	13
CAV- S06	Supply	2	3	8	22	38	16	14	13
CAV-R06	Extract	2	3	8	22	38	16	14	13
CAV- S05	Supply	2	3	8	22	38	16	14	13
CAV-R05	Extract	2	3	8	22	38	16	14	13
CAV- S01	Supply	2	3	8	22	38	16	14	13
CAV-R01	Extract	2	3	8	22	38	16	14	13

Appendix E: Calculations

Nearest residential window of dwellings along Westwells Road

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Nearest commercial window

[illegible]

Appendix F: Glossary

The list below details the major acoustical terms and descriptors, with brief definitions:

'A' Weighting

Weighting applied to the level in each stated octave band by a specified amount, in order to better represent the response of the human ear. The letter 'A' will follow a descriptor, indicating the value has been 'A' weighted. An 'A' weighted noise level may also be written as dB(A).

Airborne Noise

Noise transmitted through air.

Ambient Noise

The total noise level including all 'normally experienced' noise sources.

dB or Decibel

Literally meaning 'a tenth of a bel', the bel being a unit devised by the Bell Laboratory and named after Alexander Graham Bell. A logarithmically based descriptor to compare a level to a reference level. Decibel arithmetic is not linear, due to the logarithmic base. For example:

30 dB + 30 dB $\neq$ 60 dB

30 dB + 30 dB = 33 dB

$D_{nTw} + C_{tr}$

The weighted, normalised difference in airborne noise levels measured in a source room (L1) and a receive room (L2) due to a separating partition.

D	Is simply $L1 - L2$.
D_{nT}	Is the normalisation of the measured level difference to the expected (in comparison to the measured) reverberation time in the receiving room.
D_{nTw}	Is the weighted and normalised level difference. This value is the result of applying a known octave band weighting curve to the measured result.
C_{tr}	Is a correction factor applied to the D_{nTw} to account for the known effects of particular types of noise, such as loud stereo music or traffic noise.

Frequency (Hz)

Measured in Hertz (after Heinrich Hertz), and represents the number of cycles per second of a sound or tone.

Insertion Loss, dB

The amount of sound reduction offered by an attenuator or louvre once placed in the path of a noise level.

$L_{A90, T}$

The 'A' weighted noise level exceeded for 90% of the time period T, described or measured. The '90' can be substituted for any value between 1 and 99 to indicate the noise level exceeded for the corresponding percentage of time described or measured.

$L_{Aeq, T}$

The 'A' weighted 'equivalent' noise level, or the average noise level over the time period T, described or measured.

L_{Amax}

The 'A' weighted maximum measured noise level. Can be measured with a 'slow' (1 sec) or 'fast' (0.125 sec) time weighting.

L_{Amin}

The 'A' weighted minimum measured noise level.

NR

Noise Rating (NR) level. A frequency dependent system of noise level curves developed by the International Organisation for Standardisation (ISO). NR is used to categorise and determine the acceptable indoor environment in terms of hearing preservation, speech communication and annoyance in any given application as a single figure level. The US predominantly uses the Noise Criterion (NC) system.

Octave

The interval between a frequency in Hz (f) and either half or double that frequency (0.5f or 2f).

Pa

Pascals, the SI unit to describe pressure, after physicist Blaise Pascal.

Reverberation Time, T_{mf} , RT60, RT30 or RT20

The time taken in seconds for a sound to diminish within a room by 1,000 times its original level, corresponding to a drop in sound pressure of 60 dB. When taking field measurements and where background noise levels are high, the units RT20 or RT30 are used (measuring drops of 20 or 30 dB respectively). Sometimes given as a mid-frequency reverberation time, T_{mf} which is the average of reverberation time values at 500Hz, 1kHz and 2kHz.

R_w

The sound reduction value(s) of a constructional element such as a door, as measured in a laboratory, with a known octave band weighting curve applied to the result.

Sound Power Level

A noise level obtained by calculation from measurement data, given at the face of an item of plant or machinery. Referenced to 10^{-12} W or 1pW.

Sound Pressure Level

A noise level measured or given at a distance from a source or a number of sources. Referenced to 2×10^{-5} Pa.

Subjective Effect of Changes in Sound Pressure Level

The table below details the subjective effects of variations in sound pressures (adapted from Bies and Hansen).

Difference between background noise and rating levels	Increase in ambient noise level in 'real terms'	Change in apparent loudness
+ 10 dB	+ 10 dB	Twice as loud
+ 5 dB	+ 6 dB	Clearly noticeable
0 dB	+ 3 dB	Just perceptible
-10 dB	0 dB	No change

W

Watts, the SI unit to describe power, after engineer James Watt.